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# Effect of Co<sub>2</sub> Gas in Solar Collector Panel on Performance of Natural Circulation Domestic Solar Hot Water System

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**Abstract:** The main objective of this work is to improve the performance of conventional solar collector panel, by filling it with  $CO_2$  gas and the experiments were conducted for natural circulation system (NCS) in the months of May, August and November 2011. The performance of NCS with  $CO_2$  is compared with NCS without  $CO_2$  and the hourly average efficiency is found to be comparatively high for NCS filled with  $CO_2$ . It was inferred that the daily average system efficiency was enhanced by 3.17, 3.36 and 3.12% NCS mode of operation with  $CO_2$  filled collector panel in the months of May, August and November 2011. **Keywords:** Solar hot water system, Natural circulation mode,  $CO_2$ , Efficiency.

## 1. Introduction

In the present scenario, domestic solar hot water system requirements are increasing profoundly which prompts for advanced techniques to enhance the performance of domestic hot water system. Different methods for improving the performance of natural circulation solar hot water systems was utilised. Jaisankar et al [1] reported that by using twisted tapes, rods and spacers, there is a possibility for enhancement of heat transfer by about 10-15%. Improvement of solar absorption efficiency by an affordable solar selection coating was reported by Enab Alshamaileh [2], who observed the tank water temperature to increase by 5 °C when compared to commercial black paint coating. A 15 °C increase in tank water temperature over conventional ones was observed by Sopian et al [3] using thermoplastic natural rubber tubing as absorber plate. Muhsin Mazman et al [4] and Ella Talmatsky and Abraham Kribus [5] have studied the use of phase change materials for enhancing solar hot water system (SHWS) performance. A photovoltaic pump operated SHWS to improve the efficiency of natural circulation system by around 5-10% was investigated by Tripanagnostopoulos [6], Chow [7], Grassie et al [8], Al-Ibrahim et al [9], Kalogirou and Tripanagnostopoulos [10]. Ramasamy and Srinivasan [11] compared the performance of natural, forced and wind assisted domestic solar hot water systems. A comparative study between the performance of forced and wind assisted domestic solar hot systems was reported by Tamilarasan et al [12]. Prabu and Tamilarasan [13] have studied the performance enhancement of natural and wind assisted solar hot water systems by filling CO<sub>2</sub> gas in the collector panel. Comparison of the performance of natural and forced circulation domestic solar hot water systems by the application of green-house-effect concept were analyzed by Prabu and Tamilarasan [14]. Prabu and Tamilarasan [15] have observed the desirable effects of green-house-gas on the performance of domestic solar hot water systems.

In this study, conventional solar hot water system was operated in natural circulation mode. The efficiency of the system depends on the performance of solar collector panel used in the system. Efforts have been made to improve the performance of solar collector panel by filling it with  $CO_2$  and compared with  $CO_2$  unfilled solar collector panel in the months of May, August and November 2011. Efficiency increment was

observed in the end results for natural circulation system (NCS) due to filling of  $CO_2$  gas in the domestic solar hot water system and the same was reported in the months of May, August and November 2011.

#### 2. Experimental Setup

Two identical standard domestic solar hot water systems were fabricated each of which consisted of a solar collector plate of 2 m<sup>2</sup> area, an insulated storage tank of 200 liters capacity, insulated pipes connecting collector, tank and necessary instrumentation (Table 1). With parallel piping and valve arrangements, the system was set in NCS mode.  $CO_2$  gas was filled in the collector panel at 1 atmospheric pressure as and when required. Experiments were conducted in both the systems simultaneously to make better comparison between the two systems operated in different modes.

Platinum RTDs were used for measuring temperatures at inlet and outlet of collector and at three levels in storage tank (1/3, 1/2 and 2/3 of tank height). Dye injection technique was used for measuring the circulation rate of water. Solar radiation (both global and diffuse) were measured using calibrated PV type meter with an estimated maximum error on instantaneous collector efficiency of  $\pm$  8.1%.

Experiments were conducted on a sunny day in the months of May, August and November 2011 at Perundurai (11.32°N, 77.63°E), Erode district, Tamil Nadu state, India, and were started at 8:00 a.m. with a well-mixed tank temperature of nearly 40 °C and measurements were made at one hour interval up to 4:00 p.m. The total heat gained by tank water was calculated using initial and final well mixed tank water temperatures and also from the hourly measured data. The overall heat balance made based on hourly measured data and on the initial and final temperatures of water gave similar results (deviation within  $\pm 2.0\%$ ) in all cases.

Description	Dimension			
Initial tank water temperature	40 °C			
Time at beginning of test	8:00 a.m.			
Time at end of test	4:00 p.m.			
Day of test (NCS) & (NCS-CO <sub>2</sub> )	17 May 2011			
	15 August 2011			
	10 November 2011			
Reading interval	1 hour			
Latitude of location, Perundurai, Tamil Nadu, India	11.32°N, 77.63°E			
Collector tilt, Due south	11.32°			
Length of collector	2.1 m			
Width of collector	1.1 m			
Length of absorber plate	2.0 m			
Width of absorber plate	1.0 m			
Number of glass covers	1			
Plate to cover spacing	0.025 m			
Thickness of absorber plate	0.7 mm			
Plate absorptivity / Emissivity	0.88			
Outer diameter of collector tube	16.7 mm			
Inner diameter of collector tube	12.7 mm			
Number of tubes	8			
Tube centre to centre distance	120 mm			
Back insulation thickness	50 mm			
Side insulation thickness	43 mm			
Insulation thermal conductivity	0.04 W/m/K			
Collector fluid	Water			
Outer diameter of connecting pipes	55 mm			
Inner diameter of connecting pipes	50 mm			
Length of inlet pipe	2.1 m			
Length of outlet pipe	1.9 m			
Load pattern	No hot water is drawn			
Diameter of storage tank	0.56 m			

#### Table 1. Details of solar hot water system

Height of storage tank	0.83 m
Tank insulation thickness	50 mm
Storage tank volume	$0.2 \text{ mP}^3$

#### 3. Results and Discussion

The global- and diffuse-radiation increased during forenoon and dropped in the afternoon. With an observed variation in ambient temperature between 22.4 and 33.3 °C, the peak values of global-radiation (Ig) were between 162 and 978 W/m<sup>2</sup> and those of diffuse-radiation (Id) were between 81 and 370 W/m<sup>2</sup>.

#### **3.1 Collector Mass Flow Rate**

In NCS mode, the circulation of water through the collector took place due to thermosymphon effect. It was observed that in NCS-CO<sub>2</sub>, the circulation rate was also induced by the presence of CO<sub>2</sub> gas in the collector panel. An increase in circulation rate of water from the range of 5.64-33.92 kg/h for NCS to 7.64-35.92 kg/h for NCS-CO<sub>2</sub> was observed which could be due to the additional heat retained by CO<sub>2</sub> gas in the collector panel.

#### 3.2 Mean Tank-Water Temperature

Initial temperature of water in the tank was kept close to 40 °C at 8:00 a.m. on all the days of the experiment in order to make the comparisons easier. The water temperatures were measured at three different positions of the storage tank and an arithmetic mean was used for further calculations. Final tank water temperatures obtained in the months of May, August and November for NCS were 55.7, 50.9 and 50.9 °C, and 57.0, 52.0 and 52.1 °C for NCS-CO<sub>2</sub> modes, respectively. It was noticed that the mean tank-water temperature increases with time in all the modes of operation and highest temperature was observed in NCS-CO<sub>2</sub> mode in the month of May. As CO<sub>2</sub> retained more heat, the mean tank-water temperature was higher in NCS-CO<sub>2</sub> modes.

#### **3.3 Useful Heat Gain Rate of Water**

The variations are in line with the variation of incident solar radiation. The ranges of heat gain in the months of May, August and November for NCS were 212.36-735.30, 13.00-548.33 and 51.87-474.20 W, and 249.49-796.58, 36.24-605.17 and 75.69-520.89 W for NCS-CO<sub>2</sub> modes, respectively, which are in increasing order. Satisfactory results, in terms of relative heat gain, were obtained for NCS-CO<sub>2</sub> mode, which could be due to the increase in circulation rate of water caused by the presence of  $CO_2$  gas.

#### 3.4 Instantaneous Efficiency of the System

The instantaneous efficiency was lower at the beginning of the day, increased with time to considerable extent around 9:00-10:00 a.m. (24.00-34.77, 19.90-29.22 and 17.22-31.26%) for NCS and (27.93-38.41, 23.74-32.99 and 20.84-34.78%) for NCS-CO<sub>2</sub> modes in the months of May, August and November, and again decreased at about 4:00 p.m. (17.01, 1.72 and 6.51%) for NCS and (19.99, 4.79 and 9.50%) for NCS-CO<sub>2</sub> modes in the months of May, August and November, respectively after reaching peak values around 12:00 noon. The instantaneous efficiency obtained with NCS-CO<sub>2</sub> mode in the month of May was higher than that for other modes of operation chosen for this study.

#### 3.5 Comparison

A comparison among various modes of operation is presented in Table 2. In all the cases, the initial tank water temperature was around 40 °C. The daily average efficiency was 30.22, 25.15 and 26.06% for NCS and 33.39, 28.51 and 29.18% for NCS-CO<sub>2</sub> modes, in the months of May, August and November, respectively. The difference in relative performance among NCS and NCS-CO<sub>2</sub> modes are due to the variation in incident solar radiation and circulation rate of water through collector. The average circulation rates of water were 26.53, 21.59 and 21.83 kg/h for NCS and 28.53, 23.59 and 23.83 kg/h for NCS-CO<sub>2</sub> modes in the months of May, August and November, respectively. In general, the increase in water circulation rate (caused by the presence of CO<sub>2</sub> in NCS-CO<sub>2</sub>) resulted in increased heat gain, higher final tank-water temperature and system efficiency.

Mode & Month	Itp* (W/m <sup>2</sup> )	Ta* (°C)	Ttin (°C)	Ttend (°C)	Mc* (kg/h)	Qnet* (MJ/day)	Itpsum (MJ/day)	Qnetsum (MJ/day)	η (%)
NCS MAY	- 1384.36	30.08	40.1	55.7	26.53	13.06	44.85	13.55	30.22
NCS-CO <sub>2</sub> MAY			40.1	57.0	28.53	14.15		14.98	33.39
NCS AUGUST	- 1178.61	28.00	40.0	50.9	21.59	9.13	38.19	9.60	25.15
NCS-CO <sub>2</sub> AUGUST			40.0	52.0	23.59	10.05		10.89	28.51
NCS NOVEMBER	1117.84	26.53	40.1	50.9	21.83	9.04	36.22	9.44	26.06
NCS-CO <sub>2</sub> NOVEMBER			40.1	52.1	23.83	10.05		10.57	29.18

 Table 2. Overall performance of the system in the month of May, August and November 2011

\* - Average value over the day (8:00 a.m. – 4:00 p.m.)

### 4. Conclusions

In the present investigation, an attempt was made to improve the performance of domestic solar hot water system by applying the concept of green-house-effect. In order to estimate and improve the performance NCS, experiments were conducted before and after filling  $CO_2$  gas (at 1 atm pressure) in the collector panel of NCS. The major conclusions derived from the study are:

- 1. The system efficiency of NCS is influenced by the variation in incident solar radiation and also by the circulation rate of water through the collector.
- 2. The presence of  $CO_2$  gas in the collector panel induces the circulation rate of water in NCS- $CO_2$ .
- 3. The sequence of the systems in the increasing order of their efficiency is NCS-CO<sub>2</sub> and NCS in the months of May, November and August, respectively.
- 4. The daily average system efficiency of NCS-CO<sub>2</sub> in the month of May is higher than NCS (May, August and November) and NCS-CO<sub>2</sub> (August and November), respectively.
- 5. With a simple retrofitting type of modification (by filling CO<sub>2</sub> in the collector panel) of NCS, it can be converted into NCS-CO<sub>2</sub> which be a better and useful alternative to NCS.

### Nomenclature

Symbol	Description	Unit
NCS	: Natural circulation solar hot water system	-
NCS-CO <sub>2</sub>	: Natural circulation solar hot water system with CO <sub>2</sub> gas filled	
	in the collector panel	-
SHWS	: Solar hot water system	-
Itp	: Solar radiation on the collector plane	$W/m^2$
Itpsum	: Total solar radiation falling on the collector	MJ/day
Mc	: Mass flow rate of water across the collector	kg/h
Qnet	: Useful heat gain rate	MJ/day
Qnetsum	: Total heat gain by the tank water over the day	MJ/day
Та	: Temperature of atmospheric air	°C
Ttin	: Well-mixed tank water temperature at 08:00 a.m.	°C
Ttend	: Well-mixed tank water temperature at 04:00 p.m.	°C
η	: Daily average efficiency of the system	%

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